STRUCTURAL DESIGN WORKSHEET

• <u>Design loads</u> must be shown on construction documents:

Floor area	ı use	live load	shown	Building	is in	co	ounty	
			PSF	Ground s	now load	$P_g = \underline{\hspace{1cm}}$	PSF	(1608.2)
			PSF	Snow loa	d importa	nce factor I _s	(1608.3.3)
			PSF	Snow loa	d exposu	re factor C _e =	(1608.3.1)
			PSF	Sloped ro	oof/flat ro	of factor $C_{s=1}$		(1608.4)
Are live load reductions used? Roof thermal factor $C_t =$ (1608.3.2)							1608.3.2)	
Roof sno	w load fro	om the above	ground si	now times ac	ljustments	s is PSF	$F = P_g 0.70$	$(I_s)C_e(C_s)C_t$
		sliding or dri 108.6 to 1608	_	v locations a	nd amoun	ts are clearly	shown or	n plans and
☐ Impac (1607)		entrated load	locations	& amounts a	are shown	on plans and	l in calcul	ations
• Wind	load resis	stance design	method u	ised? ASCE	7 or <i>IB</i>	C 1609.6 Sim	plified for	r Low Rise
Amount o	of opening	s on each sid	le are: No	orth	East	_ South	Wes	st
Amount e	exterior wa	all on each si	de are: No	orth]	East	_ South	Wes	st
Is buildin	g Open, P	artially Encl	osed, or E	nclosed?		Worst case	is%	openings
		=feet		e strip calcul				-
Coefficie	nts used							
		vard Wall	Leewa	ard Wall	Windy	vard Roof	Leewa	ard Roof
C_{f}	End zone	Interior zone	End zone	Interior zone	End zone	Interior zone	End zone	Interior zone
MWFR S								
Components & Cladding								
	d importar	nce factor (I _w	(a) =	_ B	uilding us	e is importar	nce catego	ory
Exposure	terra	in is		N	orth		K _z =	=
category	terra	in is		E	ast			=
		in is			outh			=
		in is			est		$K_z =$	=
Gust effec	et factor	G =	_	Wind dir	ectionality	factor K _d =		

Earthquake design data:

Sp	ectral response coefficients S _{DS}	& S _{D1}	(1615.1)	
Sei	ismic use group Category	(1616.2)	Site Class	(1615.1.5)
Sei	ismic Design Category	(1616.3)		
•	Soil & Foundation design data:			
Al	lowable load bearing value of soil _	PSF (1804) Presumptive o	r tested? (circle one)
	Soil report is <i>provided</i> or soil repo	ort is needed (1	802.6) to verify design	
	Frost protection minimum depth of	of footings is m	et (1805.2.1).	
	Slope protection or setback is met	for footings (1	805.3).	
	Footing design & construction of J	permitted mate	rials is met (1805.4).	
	Piles or piers meet all general requ	uirements (180'	7.2.8 to 1811).	
Th	ickness & height of foundation wal	ll supporting ur	nbalanced backfill (180	5.5.1.2)
•	Concrete strength specified	psi	Designed per ACI 318	? Yes or No (circle one)
•	Masonry properties [material, thic	ckness, and typ	e (hollow or solid)]	
La	teral supports of masonry wall (210)9.4)	mortar t	ype
	Masonry veneers bonding with wa	all ties meets sp	pacing & materials? (2)	109.6.3.1)
	Anchorage of masonry to structura	al elements (ro	of or floor to masonry)	adequate? (2109.7)
	Details of bearing on masonry or o	of masonry bea	ring on other materials	(type & size needed).
	If using engineered masonry, then & 2108)	complete mase	onry calculations are to	be submitted. (2107
	Fireplaces (2111) materials, cons	truction, and ex	kterior air (2111.16) red	quirements met.
	Masonry Chimneys (2113) materi	ials, construction	on, lining, and terminat	ion requirements met.
	Flue area (2113.15 & 2113.16), m of fireblocking (2111.14 & 2113.2	•	113.14), chimney clear	rances, and locations

• Co	Steel nstruction design? LRFD (load & resistance factor) or ASD (allowable stress) or AISC-HSS
	Steel joists (2206) follow SJI specifications showing series, bearing conditions, and bracing.
	Welding (2208) and bolting (2209) details followed are noted on plans or in specifications.
	Tables 2211.1(1)&(2) steel studs shear wall values are met.
	$\frac{\text{Wood Construction}}{\text{or }No}$ Wood construction quality and labeling of materials used shown on plans as required (2303).
	Computations for sizing is based on net dimensions, not nominal member sizes (2304.2).
	Wall, floor & roof framing meets provisions of Section 2308 unless a design is specified.
	Sheathing Table 2304.6.1 (wall) and floor & roof Tables 2304.7(1), (2), (3), (4)&(5) are met.
	Follow fastener schedule 2304.9.1 for minimum number & size of nails (staples allowed).
	Heavy timber connections are properly detailed on the plans (2304.10).
	Decay and/or termite protection where required for wood (2304.11).
	es conventional light-frame construction method of Section 2308, while meeting all seven nitations: maximum 3 stories maximum 10' floor-to-floor height average dead load < 15 PSF floor live load does not exceed 40 PSF ground snow load does not exceed 50 PSF trusses do not span over 40' between supports seismic category D building meets Section 2308.12.6 limits.
Lir	mitations of wood shear walls & diaphragms to resist wind, seismic & other lateral loads meet: Principals of mechanics (2305.1.1).
	☐ Boundary elements [chord & collector framing] (2305.1.2).
	☐ Openings in shear panels (2305.1.3).
	☐ Positive shear panel connections provided (2305.1.4).
	Exception met permitting wood assembly to resist horizontal seismic forces from masonry.
	Deflection is considered in wood diaphragm designs (2305.2).

	Shear panel construction
	aphragm aspect ratio (length to width) of horizontal or sloped diaphragm is (Table 05.2.3).
Dia	aphragm aspect ratio (length to width) of shear wall diaphragm is (Table 2305.3.3).
	Shear wall width (2305.3.5) is measured between overturning restraints (2305.3.6) in load path.
	Shear wall openings clearly show force transfer around openings (2305.3.7.1) or not (2305.3.7.2).
	Summing of shear capacities has been limited per section 2305.3.8 (or an exception specified).
	Using Load and Resistance Factor design in accordance with ASCE 16? (2307)
Sec	ction 2306 Allowable Stress Design special provisions are as follows:
	Table 2306.2.1 values were substituted for 1.15 repetitive member factor for 16"o.c. 2x studs.
	Shear capacities of Table 2306.3.1 may be increased by 40% in wind design only (2306.3.1).
	Panel sheathing joints in shear walls shall occur over studs or blocking (2306.4).
	Shear capacities of Table 2306.4.1 may be increased by 40% in wind design only (2306.4.1).
	Particleboard shear walls attachment and allowable values designed per Table 2306.4.3.
	Fiberboard shear walls attachment and allowable values designed per Table 2308.9.3(4).
	Gypsum board or lath & plaster shear wall design values per Table 2306.4.5 (& Chapter 25 construction).

Instructions for STRUCTURAL DESIGN WORKSHEET

• **Design loads** must be shown on construction documents:

1607.9

structural calculations. this information, even	As the contractor, own though they may not ne	e loads must be shown or er, building inspector, ar ed the all of the calculati ur structural calculations	nd compone ions. This w	ent designers may need	atch the
Floor area use	live load shown	Building is in		county = application for	m info.
	PSF	Ground snow load	$P_g = \underline{\hspace{1cm}}$	PSF (1608.2)	
(example: Offices)	<u>50</u> PSF	Snow load importan	nce factor I	$T_{s} = $ (1608.3.3)	These are all
<u>Retail</u>	<u>100</u> PSF	Snow load exposure	e factor C _e	= (1608.3.1)	used in finding
	PSF	Sloped roof/flat roo	f factor C _s :	(1608.4)	roof
Are live load reduction	ons used? <u>NO</u>	Roof thermal factor	$C_t = $	(1608.3.2)	load, here.
Roof snow load from	n the above ground sn	ow times adjustments	isPS	$SF = P_g \ 0.7(I_s)C_e(C_s)C_t$	
☐ Unbalanced or slicalculations (160		locations and amounts	s are clearl	y shown on plans and	
-	-	be investigated to show cuctural calculations and	-		
☐ Impact or concen	trated load locations &	& amounts are shown	on plans &	calculations (1607).	
This is no change from	past practice, but just d	another reminder to clea	erly show the	ese on the plans.	
• Wind load resista	ance design method us	sed? ASCE 7 or IBC	C 1609.6 Si	mplified for Low Rise	
will come. If the secon criteria are: 1. Simple	d choice is circled, it al Diaphragm Building (a	ine from which source the so must match the criter s defined in IBC 1609.2) any of the conditions not	ia to use the and 2. not	at method. Those located on the upper	
Amount of openings	on each side are: No	rth East	South _	West	
Amount exterior wal	l on each side are: No	rth East	South _	West	
the elevations shown of operable windows, air	n the building plans. No intakes & exhaust open	terior Wall Opening Wor ote that ASCE 7 conside ings for HVAC, flexible nay be open during a de	rs (opened l & operable	by human effort) doors, louvers, gaps around	

The above question is answered by dividing the opening area by the wall area for each side and by using definitions for "Building, open" & "Building, partially enclosed" which include some minor calculations.

Is building Open, Partially Enclosed, or Enclosed? _____ Worst case is ____% openings

Coefficien		1 337 11	-	1 337 11	XX7° 1	ID C	т	ID C
C	End zone	vard Wall Interior zone	End zone	ard Wall Interior zone		vard Roof Interior zone	End zone	ard Roof Interior zone
C _f MWFR S	Liid zoiic	Interior zone	Liid Zolic	Interior zone	End zone	micrioi zone	Liid Zolic	Interior Zone
Components & Cladding								
then you si the corresp respective	hould enter ponding tab ly [for MW]	proper value bles in either FRS (Main W	s for press "ASCE 7 st ind Force	ures (in PSF) implified meth Resisting Syst	for each o hod" or "I tem) and fo	alues. If using f the above pa BC 1609.6 sin or cladding &	erts of the to aplified me component	able from thod" t pressures].
Wind load	ı importar	nce factor (I _w	,) =			se is importar	ice catego	ry
Exposure		in is			orth			=
category		in is			ast			=
		in is			outh			=
calculation	t is possible ns for wind	resisting syst	erent expos ems in the	ure factors fr building to re	esist a wind	nt wind directi I from the nort south. Depen	ions. Thus th/south di	rection
calculation could have geometry, exposure f	t is possible as for wind two differe both cases actor on the	e to have diffe resisting syst ent results, on may be neede e low wall, ca	erent expos ems in the te from the ed. For exc cusing incre	ure factors fr building to re north and on umple a mono eased girt sizi	om differentsist a wind esist a wind efrom the eslope roo ing for com	nt wind directil from the nort south. Depen f building may ponent & clau	ons. Thus th/south din ding on bu have a his dding and h	structural rection ilding gher
calculation could have geometry, exposure for MWFRS by	it is possible ins for wind to two differe both cases actor on the e more crit	e to have diffe resisting syst ent results, on may be neede e low wall, ca	erent exposems in the see from the ed. For excusing increhigh wall s	ure factors fr building to re north and on umple a mono eased girt sizi ide, even with	om different sist a wind e from the solope roofing for com	nt wind directi I from the nort south. Depen f building may	ions. Thus th/south ding on bu have a hig dding and i or.	structural rection ilding gher
calculation could have geometry, exposure for MWFRS be Gust effect All of the ca IBC 1609.	t is possible as for wind t two differe both cases actor on the e more crite ct factor above facto I simplified	e to have differesisting system tresults, on may be needeelow wall, calical from the G =	erent exposems in the seefrom the ed. For excusing incredigh wall seeffusing ASI limits on the exposers of the	ure factors fr building to re north and on umple a mono eased girt sizi ide, even with Wind dir CE 7 for design he simplified	om different sist a wind e from the solope room the lower ectionality gn, but son method mu	nt wind directi I from the nort south. Depen f building may pponent & clad exposure fact	ions. Thus th/south div ding on bu have a hig dding and i or. needed who lse that me	structural rection ilding gher have the en using the thod is not
calculation could have geometry, exposure for MWFRS by Gust effect All of the a IBC 1609. valid for u	t is possible as for wind t two differe both cases actor on the e more crite ct factor above facto I simplified	e to have differesisting system tresults, on may be neederelow wall, calical from the form th	erent exposems in the seefrom the ed. For excusing incredigh wall seeffusing ASI limits on the exposers of the	ure factors fr building to re north and on umple a mono eased girt sizi ide, even with Wind dir CE 7 for design he simplified	om different sist a wind e from the solope room the lower ectionality gn, but son method mu	nt wind directive from the norm south. Dependent & classification of the control	fons. Thus th/south div ding on bu have a his dding and i for. needed who lse that me he full ASC	structural rection ilding gher have the en using the thod is not
calculation could have geometry, exposure for MWFRS because effect All of the call of the call for under the call for under the call for under the call for t	t is possible as for wind t two differe both cases actor on the e more crit ct factor above facto I simplified se, thus it v	e to have differesisting system tresults, on may be neederelow wall, calical from the form th	erent exposems in the tend. For examples increased in the tendent	ure factors fr building to re north and on umple a mono eased girt sizi ide, even with Wind dir CE 7 for design he simplified	om different sist a wind e from the solope room the lower ectionality gn, but son method mu	nt wind directify from the norm south. Dependent & classification of the control	ions. Thus th/south ding on bu have a hig dding and h or. meeded who lse that me he full ASC	structural rection ilding gher have the en using the thod is not EE 7 design.
calculation could have geometry, exposure for MWFRS by Gust effect All of the call of the	it is possible ins for wind it two differe both cases factor on the e more crite ct factor above facto I simplified se, thus it we requake de-	e to have differesisting system tresults, on may be needeelow wall, calical from the G = rs will apply if method. All will be rejected sign data:	erent exposems in the tend from the tend. For example, wall so the tendent of the	ure factors from the building to reserve to morth and on the amono eased girt sizing ide, even with the Wind direct of the simplified the simplified the simplified to the wiewer and with the simplified	om different esist a wind e from the solope room the lower ectionality gn, but son method muwill require (161)	nt wind directify from the norm south. Dependent & classification of the control	tons. Thus th/south ding on but have a high ding and it or. meeded who lise that me he full ASC ap values of re taken for see 2 values	structural rection ilding gher have the ren using the thod is not $S_S \& S_1$ in the the location
calculation could have geometry, exposure for MWFRS by Gust effect All of the call IBC 1609. valid for use Earth Spectral respectively.	it is possible ins for wind it two differe both cases factor on the e more crite ct factor above facto I simplified se, thus it we requake de-	e to have differesisting system results, on may be needed to wall, call from the first will apply in the first will apply in the first will be rejected to sign data: Category	erent exposems in the tend. For example, wall stands with the tender of	ure factors from the building to reserve to morth and on the amono eased girt sizing ide, even with the Wind directly consistent of the simplified eviewer and very signification.	om different esist a wind e from the solope room the lower ectionality gn, but son method muwill require (161)	at wind directiful from the norm south. Dependent & class for the properties of the	fons. Thus th/south ding on bu to have a his dding and h tor. meeded who lse that me the full ASC ap values of re taken for ese 2 values (16	structural rection ilding gher have the en using the thod is not $EE 7$ design. S _S & S ₁ in the the location are calculated.

The last blank to fill-in is the <u>Seismic Design Category</u>, this is the most important. The information found in the other four blanks is used to determine that category. If the Design Category is A, then no further seismic design calculation is required for your building. Further design is needed for categories B to F. Exception: IBC Section 1615.1 provides that structures located north of the 4%g contour line as shown in IBC Figure 1615(2) or in COMM Figure 62.16-2 [alternate 4%gcontour line] shall be assigned to Seismic Design Category A and need only comply with the requirements of Section 1616.4.

•	This value is found by soil test, submit = a copy or else by IBC Table 1804.2.
Λ 1°	owable load bearing value of soil PSF (1804) Presumptive or tested? (circle one)
AL	
Ц	Soil report is <i>provided</i> or soil report is <i>needed</i> (1802.6) to verify design. Plan reviewer will likely question any
	Frost protection minimum depth of footings is met (1805.2.1).
	Slope protection or setback is met for footings (1805.3).
	Footing design & construction of permitted materials is met (1805.4). The code contains many empirical
	Piles or piers meet all general requirements (1807.2.8 to 1811).
Th	ckness & height of foundation wall supporting unbalanced backfill (1805.5.1.2)
	of the check boxes above are provided for the designer to verify that he or she has thought of each of se items, as code officials may be looking at these in reviews & inspections.
•	<u>Concrete</u> strength specifiedpsi Designed per ACI 318? <i>Yes</i> or <i>No</i> (circle one)
Th	s basic information is needed in the calculations, but also on the plans or in a specification book.
•	Masonry properties [material, thickness, and type (hollow or solid)] List here all that apply.
La	eral supports of masonry wall (2109.4) <u>The supports of mortar type</u> mortar type
	Masonry veneers bonding with wall ties meets spacing & materials? (2109.6.3.1)
	Anchorage of masonry to structural elements (roof or floor to masonry) adequate? (2109.7)
	Details of bearing on masonry or of masonry bearing on other materials (type & size needed).
	of the check boxes above are provided for the designer to verify that he or she has thought of each of see items, as code officials may be looking at these in reviews & inspections.
	If using engineered masonry, then complete masonry calculations are to be submitted. (2107 & 2108)
inc des	building designer is responsible for masonry fireplace and masonry chimney design, thus it must be uded in the initial building plan design and calculation submittal. This is not something that an HVAC igner could submit at a later date, as all structural requirements are ultimately the building designer's ponsibility. Building designer can & should work together with HVAC designer on the need for these.
	Fireplaces (2111) materials, construction, and exterior air (2111.16) requirements met.
	Masonry Chimneys (2113) materials, construction, lining, and termination requirements met.
	Flue area (2113.15 & 2113.16), multiple flues (2113.14), chimney clearances, and locations of fireblocking (2111.14 & 2113.20) are met.

• <u>Steel</u> Construction design? <i>LRFD</i> (load & resistance factor) or <i>ASD</i> (allowable stress) or <i>AISC-HS</i>	S
By circling one of the above will indicate which method was used in your calculations.	
☐ Steel joists (2206) follow SJI specifications showing series, bearing conditions, and bracing	Ţ .
☐ Welding (2208) and bolting (2209) details followed are noted on plans or in specifications.	
☐ Tables 2211.1(1)&(2) steel studs shear wall values are met.	
Each of these above 3 check boxes serve as a reminder to designers to show adequate detail on the plan	s.
Wood Construction Yes or No Wood construction quality and labeling of materials used shown on plans as required (2303)).
☐ Computations for sizing is based on net dimensions, not nominal member sizes (2304.2).	
The above two check boxes apply to all wood construction. The next one refers to empirical method of section 2308, which can only be used where meeting seven limitations noted below. Each of the five following may or may not apply to the building design, depending on construction method proposed.	
☐ Wall, floor & roof framing meets provisions of Section 2308 unless a design is specified.	
☐ Sheathing Table 2304.6.1 (wall) and floor & roof Tables 2304.7(1), (2), (3), (4)&(5) are me	t.
☐ Follow fastener schedule 2304.9.1 for minimum number & size of nails (staples allowed).	
☐ Heavy timber connections are properly detailed on the plans (2304.10).	
☐ Decay and/or termite protection where required for wood (2304.11).	
Uses <i>conventional light-frame construction</i> method of Section 2308, while meeting all seven limitations: □ maximum 3 stories □ maximum 10' floor-to-floor height □ average dead load < 15 PSF □ floor live load does not exceed 40 PSF □ ground snow load does not exceed 50 PSF □ trusses do not span over 40' between supports □ seismic category D building meets Section 2308.12.6 limits.	

Use of this empirical method noted above, when applicable, will not require structural calculations. But the plans will then be required to clearly have the specifications and details needed to show that each of the tables for members used and the connection minimums are properly & clearly provided on the plans.

The next requirement deals with wood construction using a diaphragm system for horizontal load resistance. If a rigid frame or braced frame resisting system is used instead of a diaphragm system, then that must be clearly shown in the structural calculations and adequate connection details on the plans. The Lateral Load Resisting System & Connection Worksheet should be used in addition to this checklist to clearly show how compliance with all code requirements is being provided.

Wo	ood shear walls & diaphragms to resist wind, seismic, and other lateral loads limitations of: Principals of mechanics (2305.1.1).
	☐ Boundary elements [chord & collector framing] (2305.1.2).
	☐ Openings in shear panels (2305.1.3).
	☐ Positive shear panel connections provided (2305.1.4).
	Exception met permitting wood assembly to resist horizontal seismic forces from masonry.
	Deflection is considered in wood diaphragm designs (2305.2).
	Shear panel construction
	aphragm aspect ratio (length to width) of horizontal or sloped diaphragm is (Table 05.2.3).
Dia	aphragm aspect ratio (length to width) of shear wall diaphragm is (Table 2305.3.3).
	Shear wall width (2305.3.5) is measured between overturning restraints (2305.3.6) in load path.
	Shear wall openings clearly show force transfer around openings (2305.3.7.1) or not (2305.3.7.2).
	Summing of shear capacities has been limited per section 2305.3.8 (or an exception specified).
the. bui	of these above requirements for diaphragm construction are of concern to code officials. Most of se requirements will be needed to be verified to plan examiners, but some may also be questioned by lding inspectors. As such, if the compliance is clearly shown on the plans, both code officials will be the information at their fingertips. This saves time for contractors, designers & code officials alike.
	Using Load and Resistance Factor design in accordance with ASCE 16? (2307)

Sec	ction 2306 Allowable Stress Design special provisions are as follows:
	Table 2306.2.1 values were substituted for 1.15 repetitive member factor for 16"o.c. 2x studs.
	Shear capacities of Table 2306.3.1 may be increased by 40% in wind design only (2306.3.1)
	Panel sheathing joints in shear walls shall occur over studs or blocking (2306.4).
	Shear capacities of Table 2306.4.1 may be increased by 40% in wind design only (2306.4.1)
clea	te that when these above substitutions or increases are being used in your calculations, it will help to arly label where & what increase is being used or substitution is being made (to verify that it is plicable to the place where it is used).
	Particleboard shear walls attachment and allowable values designed per Table 2306.4.3.
	Fiberboard shear walls attachment and allowable values designed per Table 2308.9.3(4).
	Gypsum board or lath & plaster shear wall design values per Table 2306.4.5 (& Chapter 25 construction).

These last three check boxes are cautions for the designer using them. If these non-standard materials are used for wind resisting elements, then the framing & connections must meet all the limitations placed on them by the table headings or footnotes. Plans must clearly indicate adequate load paths for them.